

The use of pulse shape in PD testing of cable systems at VLF

ICC – PES, Sub. F, Fall 2010 Meeting, Scottsdale/Fountain Hills, AZ

High-pot VLF testing of power cable systems is widely used for condition assessment of Medium Voltage networks:

- ❑ Combined PD and VLF test spots the presence of local defects which may not break down the insulation during the high-pot test;**
- ❑ PD testing at VLF requires advanced noise rejection techniques to be employed**

Under VLF voltage :

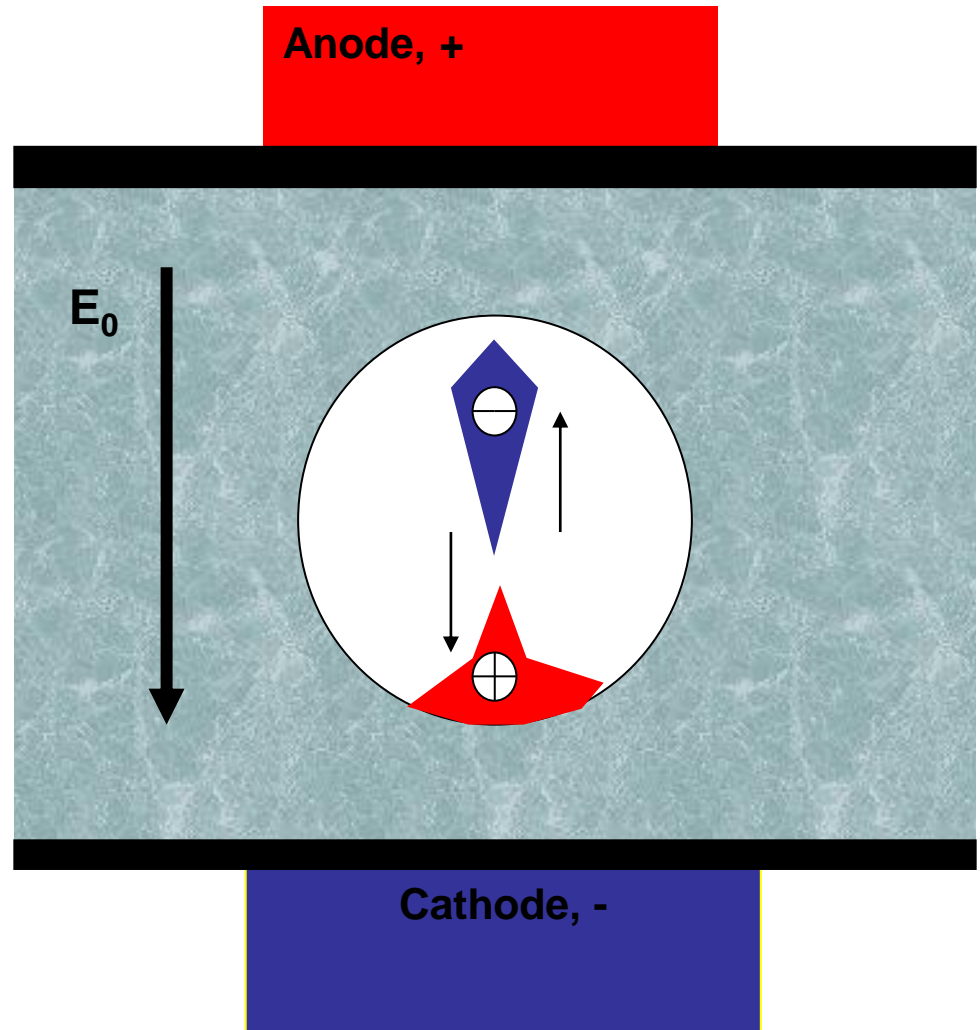
- ❑ Internal PD have much smaller repetition rate,**
- ❑ electromagnetic noise and external disturbances are present as well**

What happens during a PD? (1)

Let's start with a little bit of physics:

The PD transfers:

- Electrons to the cavity surface acting as anode
- Positive ions to the cavity surface acting as cathode



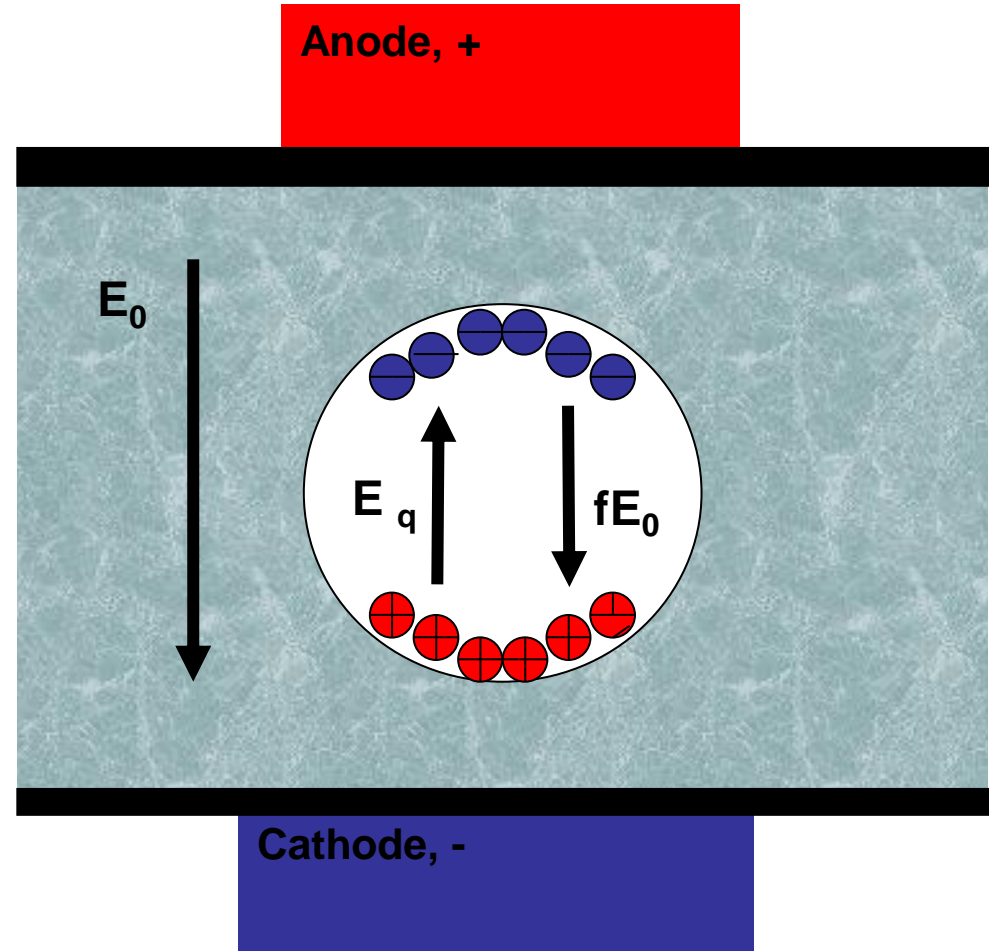
What happens during a PD? (2)

This charge distribution generates a **local field** E_q

The local field has opposite sign to the **external field** (i.e., due to the external source), fE_0 .

Thus, the local field reduces the **internal field** (i.e., the field inside the cavity).

$$E_i = fE_0 - E_q$$



Main differences between PD under DC and AC

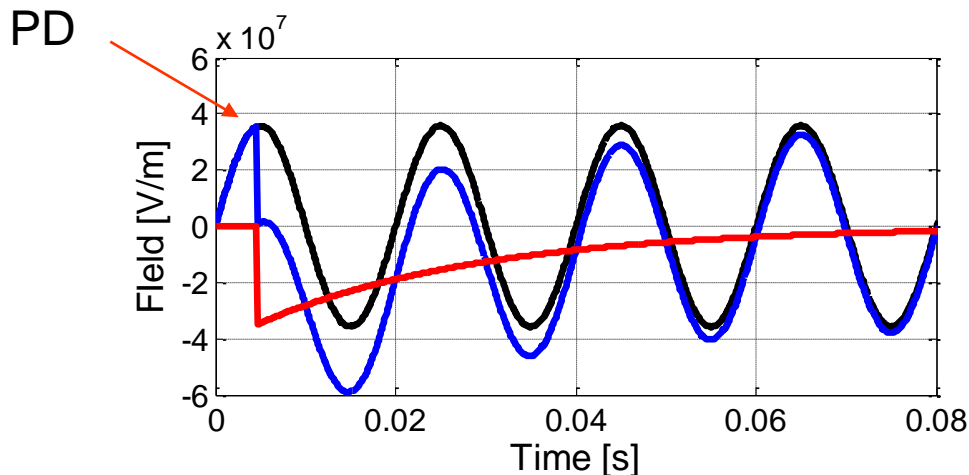
Space charge generated electric field

The charge deployed by previous discharge activity, q_{SC} , decays by processes such as drift along the cavity walls, diffusion into the dielectric bulk and neutralization. In a first approximation:

$$q_{SC} = q_{SC0} \cdot e^{-\Delta t/\tau};$$

q_{SC0} = Space charge just after the last PD
 Δt = Time elapsed since the last PD
 τ : = Time constant

Example: $\tau=25\text{ms}$; Voltage frequency = 50 Hz.



$f_A \cdot E_0$ = Background field

E_q = Space-charge-generated electric field

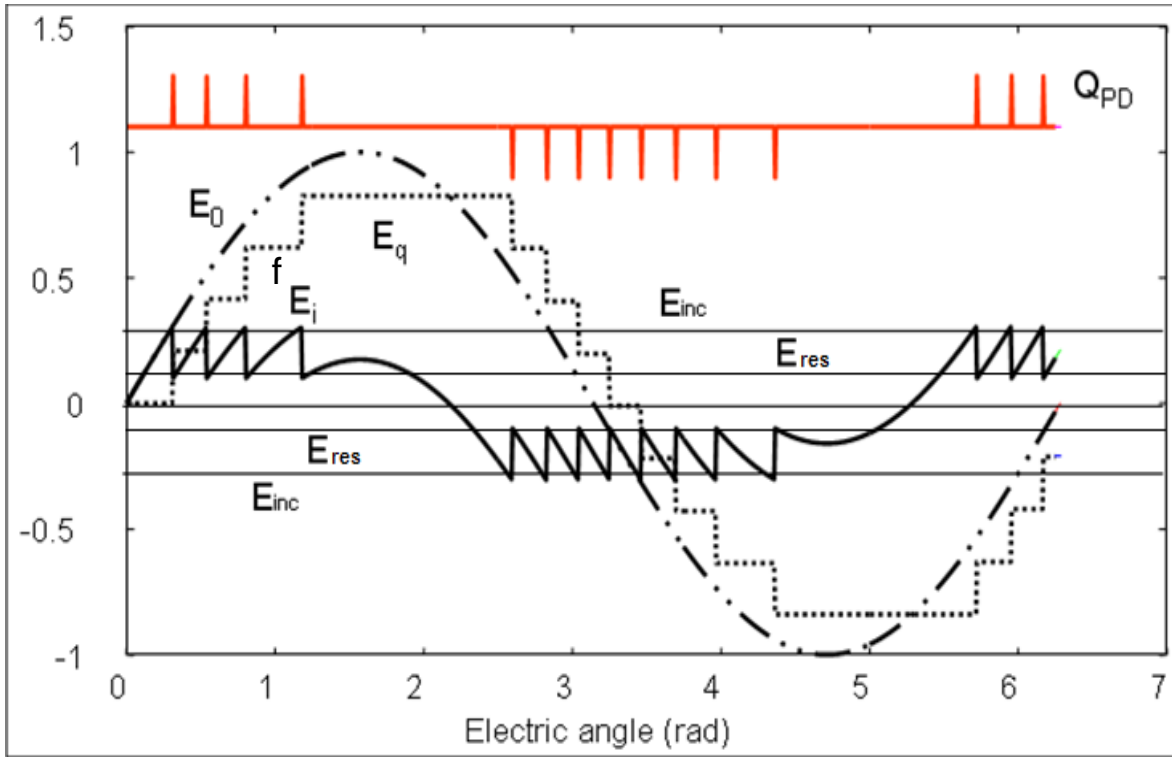
E_i = Field inside the cavity

Main differences between PD under DC and AC

Simplistic PD description

Hypotheses:

- Infinite electronic availability (PD always occurs when $E_i = E_{inc}$)
- No charge diffusion (E_q constant between subsequent PD)

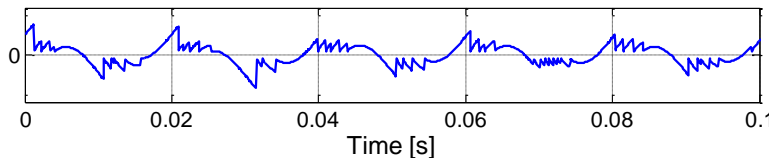
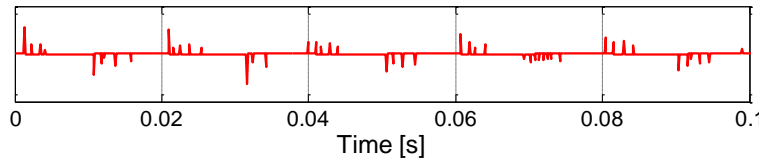


- E_{inc} , inception field
- E_{res} , residual field
- $fE_0 = fE_{max} \sin(2\pi \text{freq} \cdot t)$, field due to the applied voltage.
- E_q , local field, due to the charge distribution, changes after each PD.
- $E_i = fE_0 - E_q$, total field inside the cavity

Main differences between PD under DC and AC

AC or varying voltage:

- Sinusoidal voltage at industrial frequency → Repetition rate is generally higher than under DC (up to hundreds of pulses per second), due to:



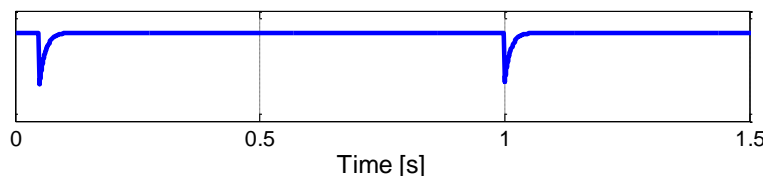
- Time varying background field;
- Polarity inversions;

I_{PD} = PD current pulses

E_i = Field inside the cavity

DC:

- Voltage constant → Low repetition rate (typically one discharge per second or less)



- Charge from previous PD reduces the internal field;
- No polarity inversions;

I_{PD} = PD current pulses

E_i = Field inside the cavity

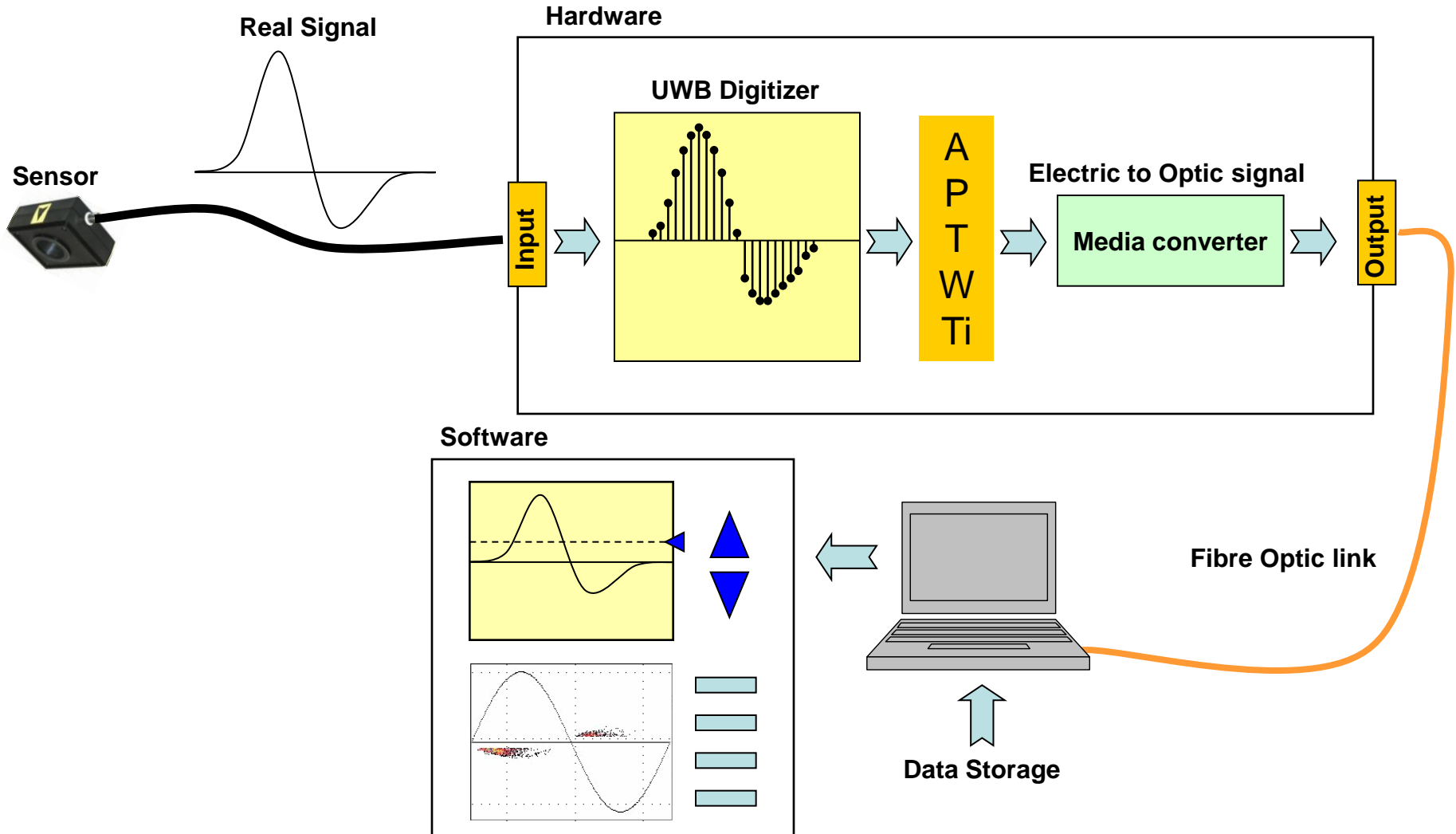
ULTRA WIDE BAND APPROACH FOR PARTIAL DISCHARGES MEASUREMENTS

Ultra Wide Band acquisition allows:

- **Classification by “Time – Frequency” mapping of acquired pulses**
 - **Phenomena separation (Noise, Disturbances, Multiple PD activities, etc.)**
 - **Real-time Noise rejection based on pulse shape characteristics**
 - **Single phenomenon identification**
 - **Localization (various techniques)**
- It can be applied on-line, off-line at power frequency, RTS and VLF**

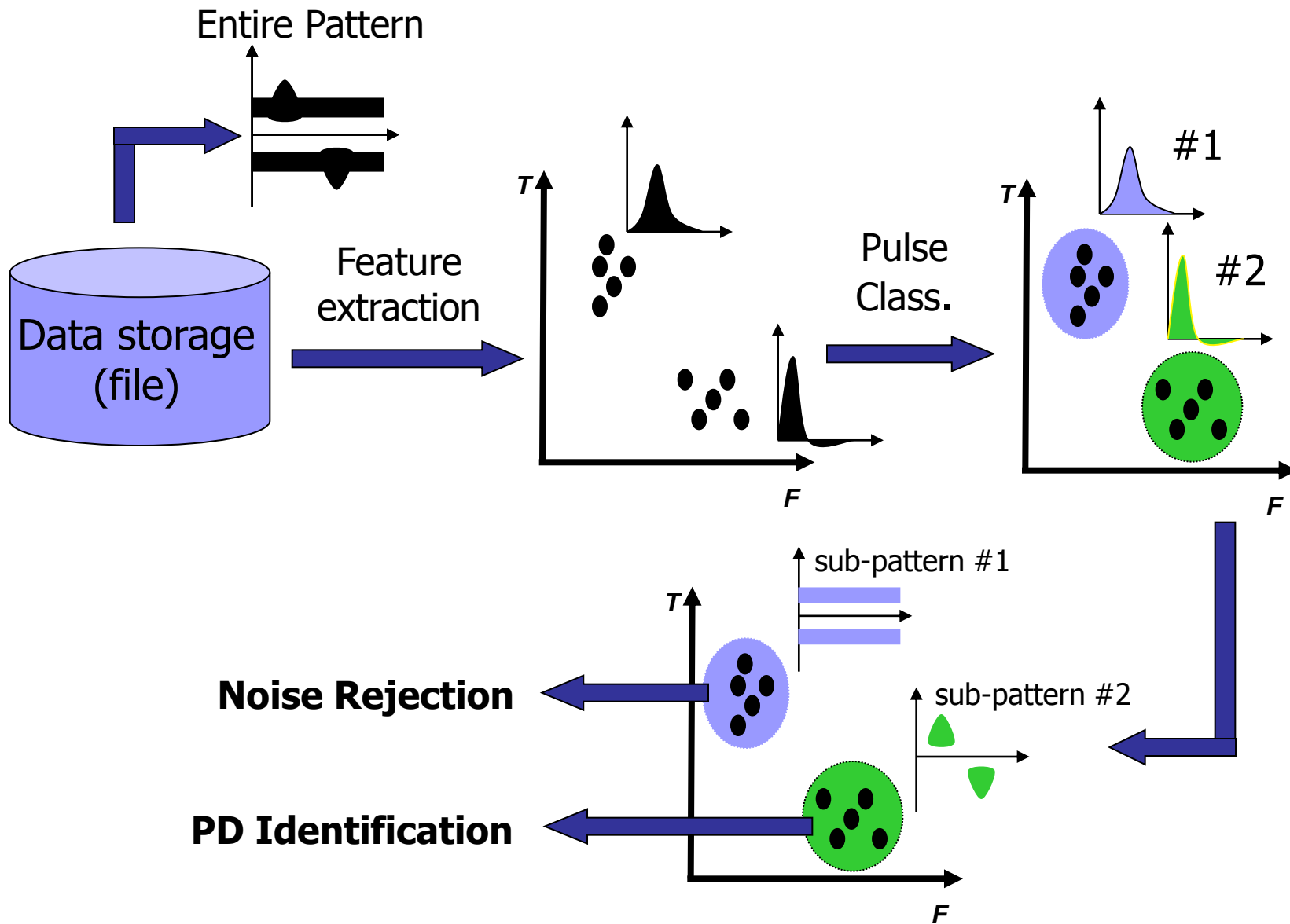
Separation

Innovative diagnostics by means of PD measurements: System Layout



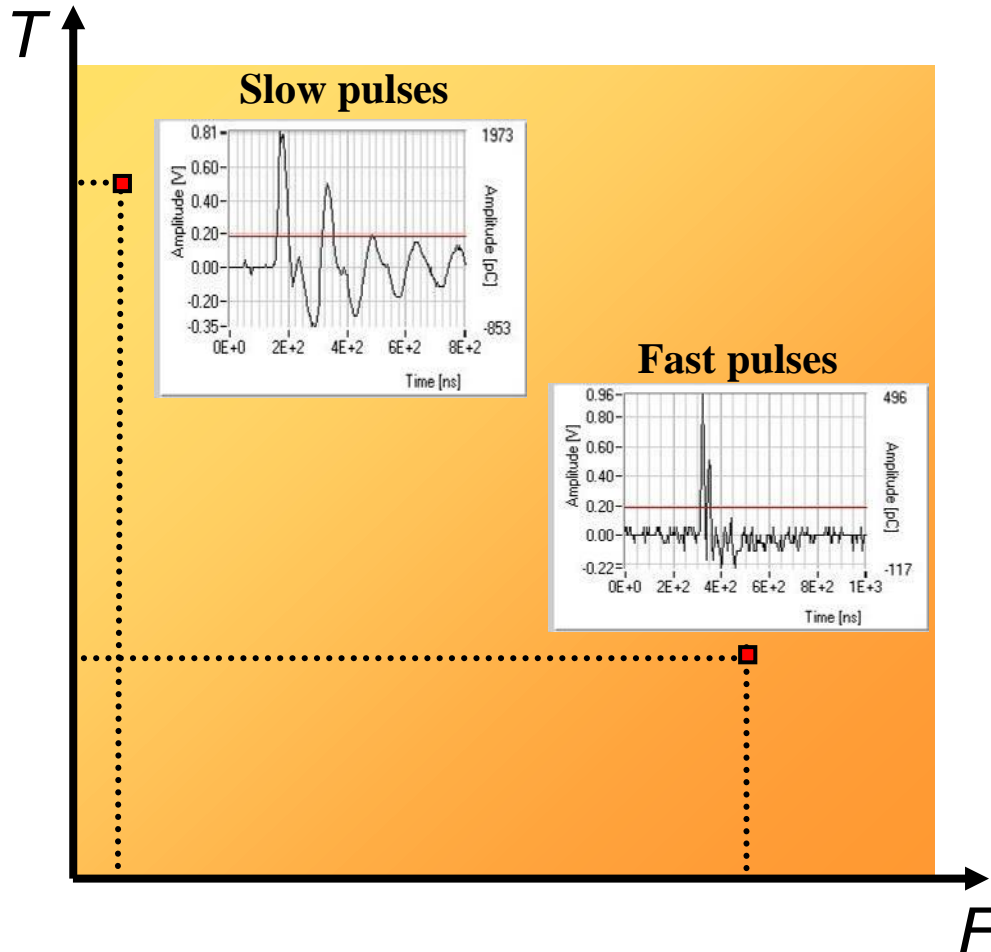
Separation

Innovative diagnostics by means of PD measurements: Data Flow



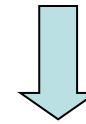
Classification by T-F mapping

Each acquired pulse is represented with 2 parameters



Normalization of the pulse

$$\tilde{s}(t) = s(t) / \sqrt{\int_0^L s(\tau)^2 d\tau}$$

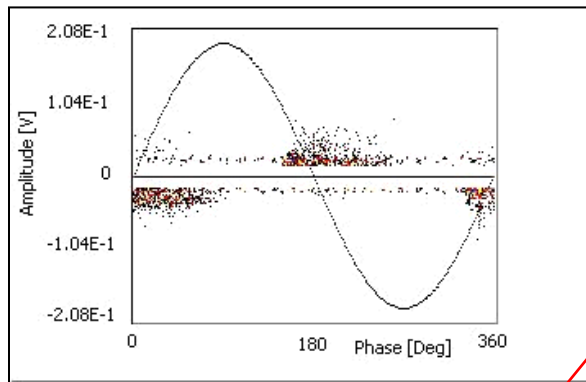


$$\left\{ \begin{array}{l} t_0 = \int_0^L t \tilde{s}(t)^2 dt \\ T = \sqrt{\int_0^L (t - t_0)^2 \tilde{s}(t)^2 dt} \\ F = \sqrt{\int_0^\infty f^2 |\tilde{S}(f)|^2 df} \end{array} \right.$$

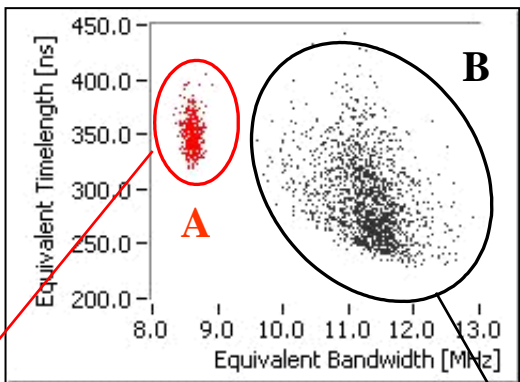
$S(f)$ is the Fourier transform of s
 L = time length of the pulse

Example of data processing #1

Entire PD pattern

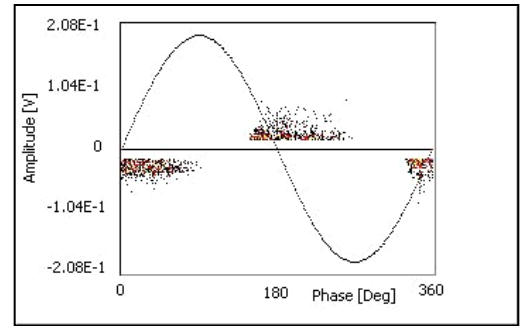


T-F Map

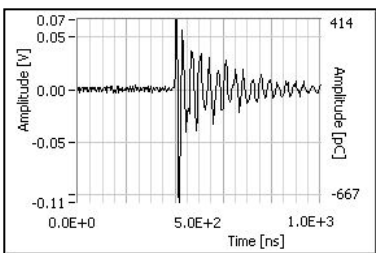


A

Sub-pattern A



Waveform A

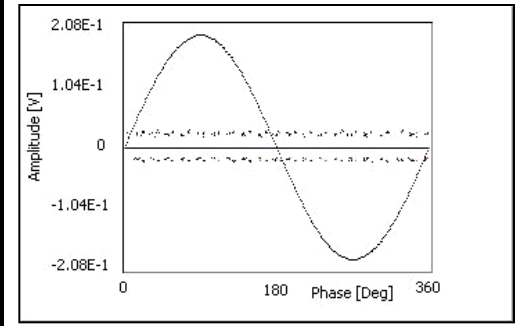


TECHIMP First ID Level

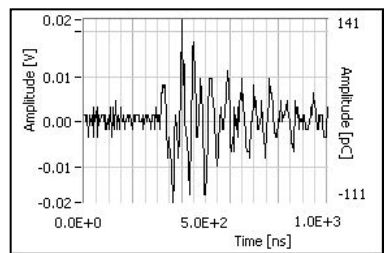
- Corona Discharges: 0.00
- Surface Discharges: 0.00
- Internal Discharges: 1.00
- Invalid Data: 0.00
- Noise: 0.00

B

Sub-pattern B



Waveform B



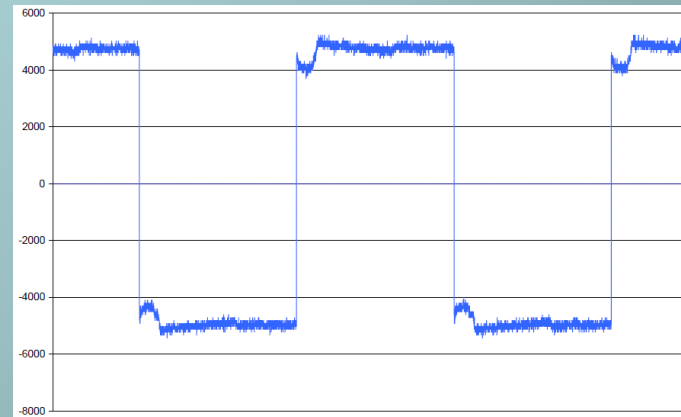
TECHIMP First ID Level

- Corona Discharges: 0.00
- Surface Discharges: 0.00
- Internal Discharges: 0.00
- Invalid Data: 0.00
- Noise: 1.00

Case Study #1: MV feeder, VLF off-line PD test

Apparatus: Medium voltage cable feeder
Voltage level: 15 kV
Location: USA

T-F map separation allows PD phenomena to be detected during off-line VLF tests performed with **cosine-rectangular** voltage



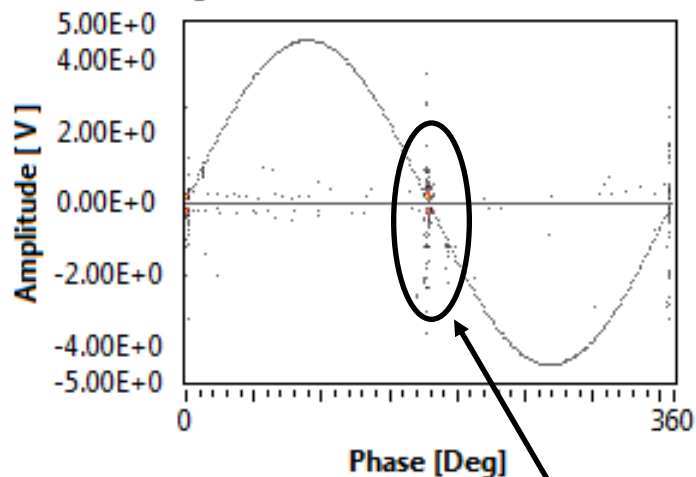
2. Dry test

Step 1: Dry test

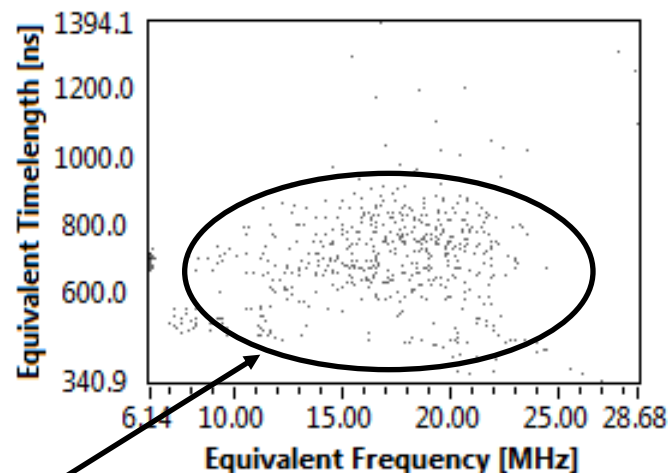
- The VLF supply is energized with no cable connected;
- PD phenomena coming from the VLF are acquired (VLF supply fingerprint)

Results:

Partial Discharge Pattern



Classification Map



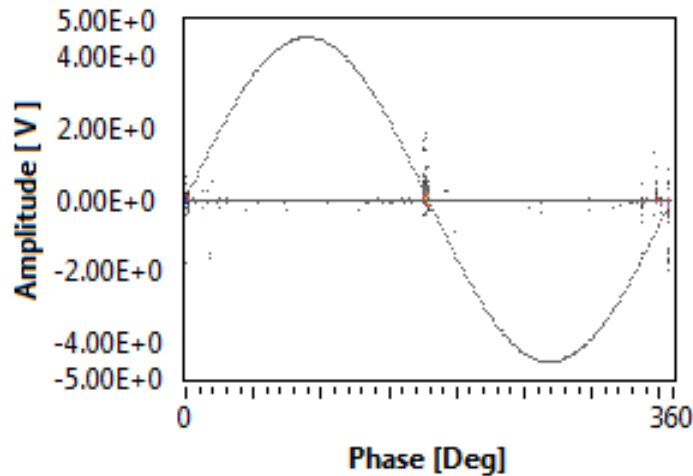
PD from the VLF supply

3. PD test

Step 2: PD test

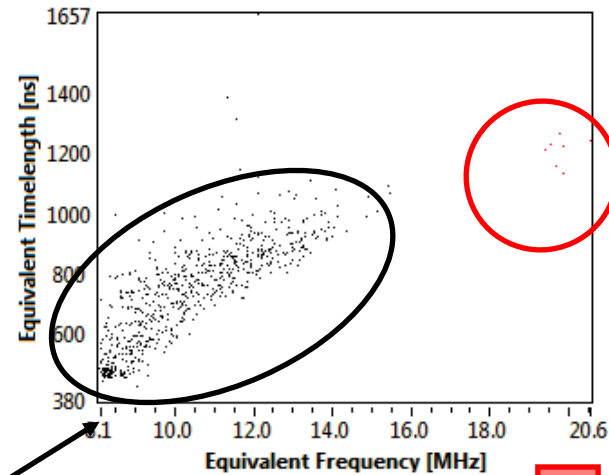
- The feeder is connected to the VLF supply;
- New PD phenomena can be acquired and recognized as coming from the EUT (cable feeder)

Partial Discharge Pattern



PD from the VLF supply

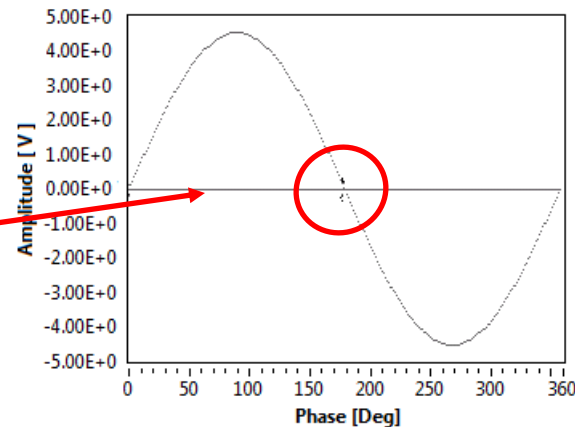
Classification Map



Separation

PD coming from the EUT

Partial Discharge Pattern



Case Study #2: MV feeder, on-line and VLF off-line PD test

Apparatus: Medium voltage cable feeder
Voltage level: 14kV
Location: USA

Application of PD phenomena separation by
T-F mapping, on-line and at sinusoidal VLF

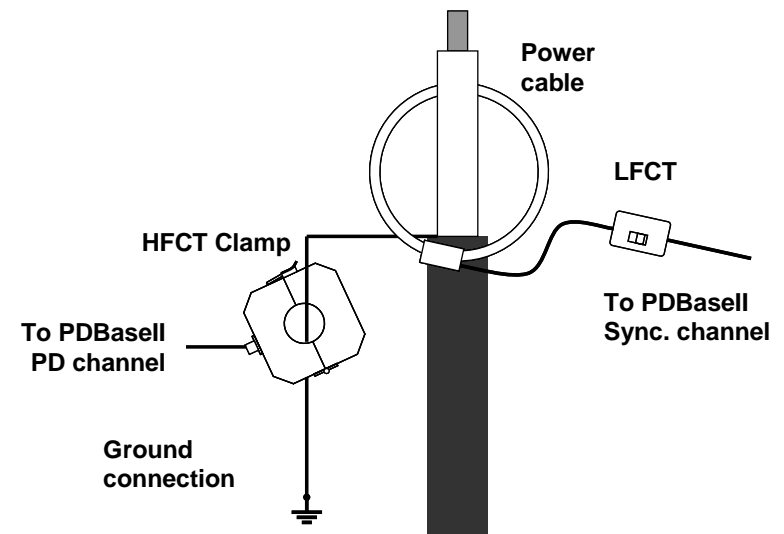
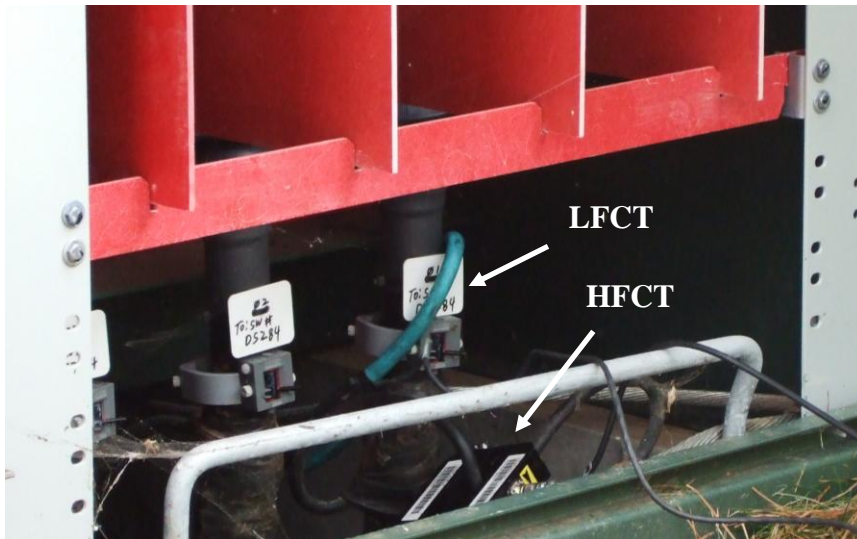
1. Measurement Setup

PD signals:

HFCT (High Frequency Current Transformer) clamped around the ground lead of the cable termination

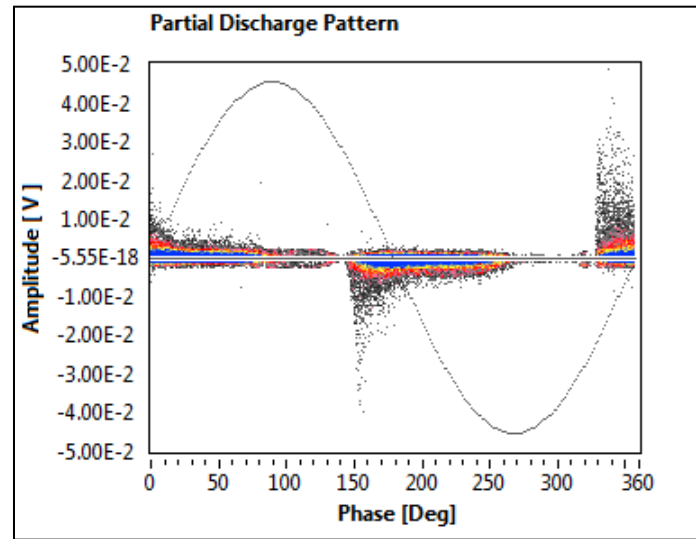
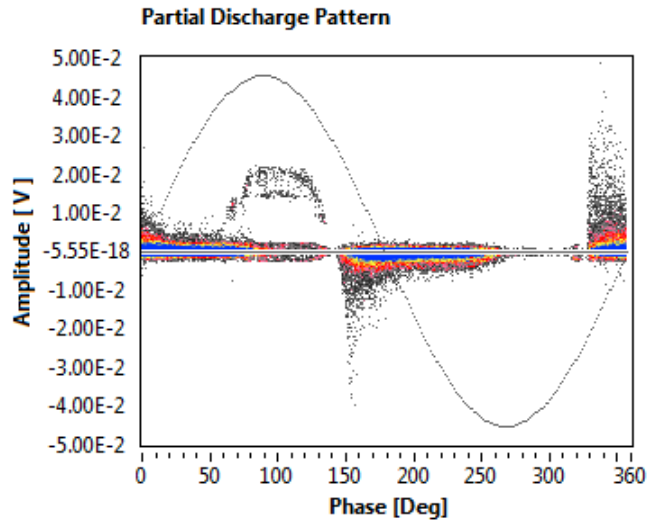
Synchronization signal:

- ❑ through a Low Frequency Current Transformer clamped around the cable termination for on-line measurement
- ❑ through a capacitive divider for the off-line VLF test

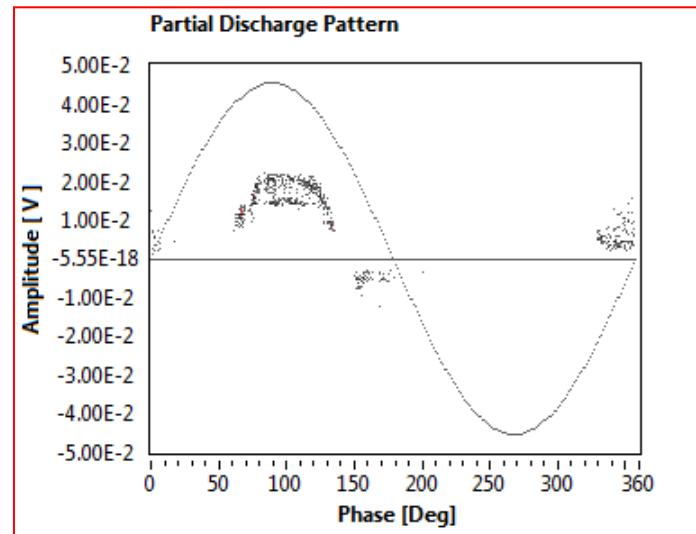
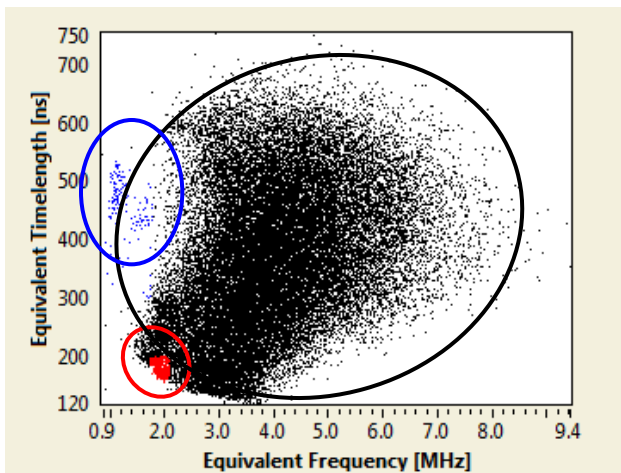


2. On-line test

**Step 1: On-line 14kV (phase to ground) @ 60 Hz;
Feeder supplied by the grid (no loads connected)**



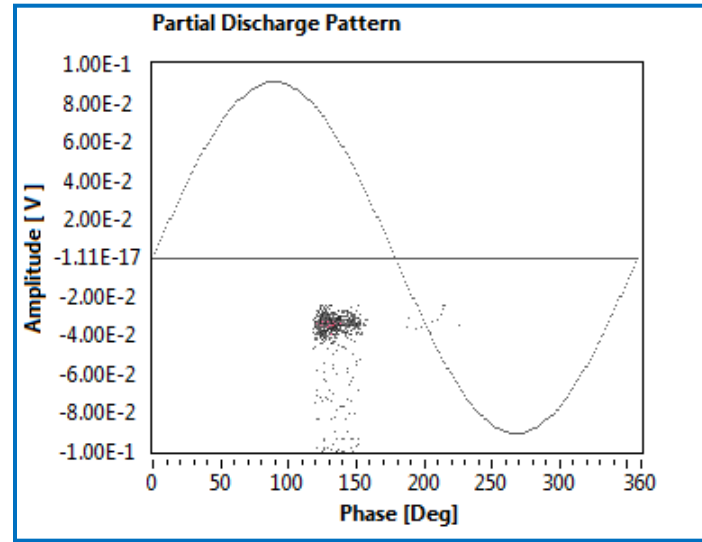
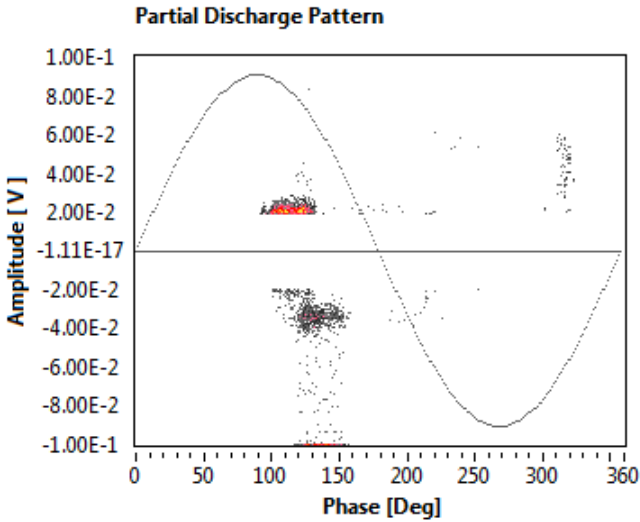
**Internal PD
(black cluster
high repetition
rate)**



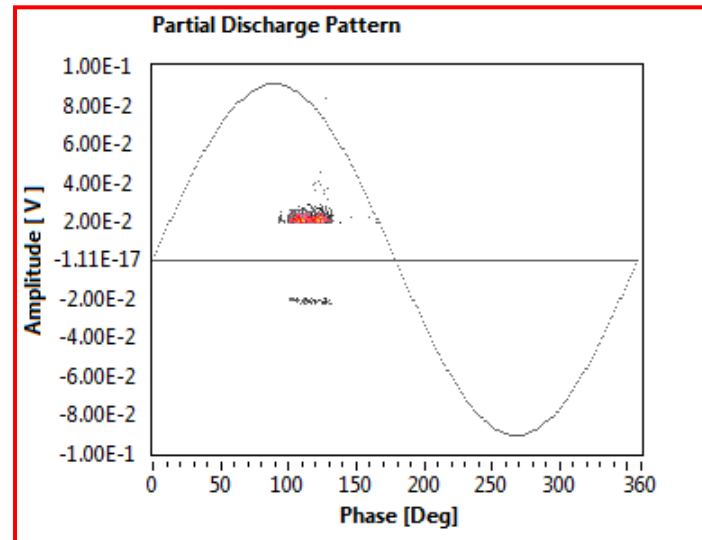
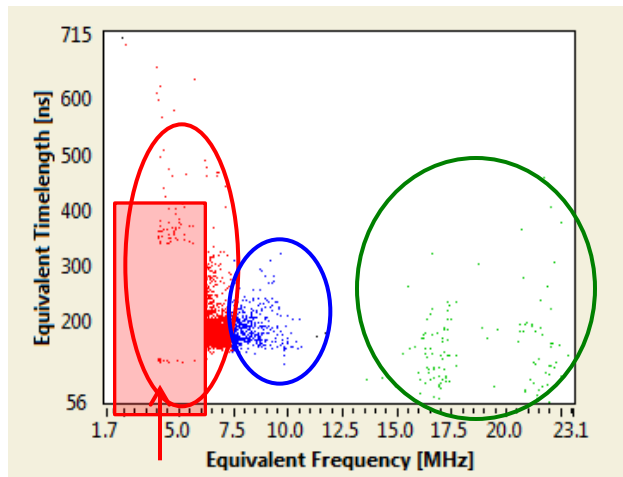
**Corona PD
(red cluster,
low
repetition
rate)**

3. Off-line VLF test

Step 2: Off-line 23kV (phase to ground) @ 0.1 Hz;
0.1 Hz sine-wave compact VLF unit



Internal PD
(blue cluster)



Corona PD
(red cluster)

Real-time filter

- The decomposition of the pulse frequency and time characteristics allows:
 - Enhanced noise rejection
 - PD **separation**
 - PD **location**
 - PD source **identification** by artificial intelligence methods
- Real-time pulse selection based on PD pulse characteristics (in time and frequency domains) allows separation of signals coming from different sources to be performed, in order to focus on PD activity coming from the cable system under test

Thank you !